

# A Comprehensive Study on Interface Perpendicular MTJ Variability

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Spin transfer torque MRAM (STT-MRAM) is one of the promising candidates as a scalable nonvolatile memory with high density, and CMOS compatibility [1], [2]. Interface perpendicular magnetic tunnel junction (PMTJ) shown in Fig. 1 has been demonstrated with the goal of reducing the switching current while maintaining sufficient nonvolatility [3]. However, previous studies report that PMTJ suffers from process-dependent dimensional variations, thus it remains one of the major constrains in achieving high performance STT-MRAM [4, 5]. As shown in the equations of Fig. 1, the anisotropy field ( $H_K$ ) and free layer volume ( $V$ ) are functions of PMTJ dimensions, hence their variations result in variation of STT switching characteristics such as thermal stability factor ( $\Delta$ ) and switching current ( $I_C$ ). The  $H_K$  of PMTJ has a strong dependency on relative ratio between the free layer thickness ( $t_F$ ) and the critical thickness ( $t_C$ ) [3]. The equations of Fig. 1 suggest that the  $t_F$  variation differently affects the PMTJ dimension-dependent parameters (gray circles), resulting in either increasing or decreasing  $\Delta$  and/or  $I_C$ . This paper presents a comprehensive study on process-dependent dimensional variability of PMTJ, especially focusing on estimating the impact of  $t_F$  variation on  $\Delta$  and  $I_C$  variability. For a practical analysis, our physics-based macrospin SPICE model [7] captures the key physics of STT switching in PMTJ by incorporating all of the above mentioned PMTJ dimension-dependent parameters into the Landau-Lifshitz-Gilbert (LLG) equation.

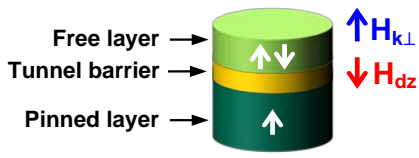
The variation factors and realistic PMTJ material parameters [3], [5], [6] used in this work are listed in Table 1. Our variability analysis is based on determining the degree of  $\Delta$  for a target chip failure rate. Here, we assume a STT-MRAM L3 cache with 64MB density for server processor as a target memory system. The  $7.95 \times 10^{-7}$  chip failure rate is set by the repair capability and corresponding  $\Delta$  of 70 for 10 years of retention is estimated [8]. A double MgO interface [5] is considered to scale the  $I_C$  down and increase the  $\Delta$  for meeting the system specification. The  $t_F$ -dependent damping factor ( $\alpha$ ) in CoFeB is also considered for realistic analysis. To estimate the impact of process-dependent dimensional variations on PMTJ variability, appropriate values of the variation ( $3\sigma/\mu$ ) in the free layer width and length are set to 12% according to the ITRS roadmap. Moreover, the variation ( $3\sigma/\mu$ ) of  $t_F$  is varied from 4% to 9% with 1% step to evaluate its dependency on  $\Delta$  and  $I_C$  variability. Each variation parameter is assumed to have a normal distribution with  $\pm 3$  standard deviation ( $\sigma$ ). The Monte Carlo simulator extracts the 1000 random variables with  $\pm 3\sigma$  for all the above mentioned dimension-dependent parameters, then, our simulation model estimates each  $I_C$ ,  $\Delta$ , and  $t_{\text{retention}}$  variability for a given switching time ( $t_{\text{sw}}$ ).

Fig. 2(a) shows the simulated  $I_C$  as a function of  $t_{\text{sw}}$  at 50% switching probability. Note that our model demonstrates realistic dynamic spin motions based on measured data [9]. A constant  $t_{\text{sw}}$  of 5ns was chosen for following variability simulations. As shown in Figs. 2(b) and 3, each  $I_C$ ,  $\Delta$ , and  $t_{\text{retention}}$  variability has Gaussian distribution under free layer  $W$ ,  $L$  variation of 12% and  $t_F$  variation of 4%. Fig. 4 shows the  $t_F$  variation dependency on  $\Delta$  variability. Simulation result indicates that the  $\Delta$  variability has a strong linear dependency on  $t_F$  variation. Variability trend of  $t_{\text{retention}}$  is projected directly from the variability trend of  $\Delta$  [5]. Fig. 5 shows correlation maps between  $t_{\text{retention}}$  and  $I_C$  variability under different  $t_F$  variation conditions (4%, 9%). It offers a clear comparison of impact of  $t_F$  variation on  $t_{\text{retention}}$  and  $I_C$  variability. The slope ( $\Delta I_C / \Delta t_{\text{retention}}$ ) difference suggests that the  $t_{\text{retention}}$  variability has a stronger dependency on  $t_F$  variation compare to  $I_C$  variability counterpart. Moreover, over 40% Monte Carlo random samples do not meet a retention time of 10 years for both different  $t_F$  variation cases. Increasing  $\Delta$  shown in Fig. 6 would be considered to make all of random samples meet a target of 10 years retention [10]. However,  $I_C$  increase is unavoidable for increasing  $\Delta$ . After increasing  $\Delta$ , the correlation maps are replotted in Fig. 7 compared to Fig. 5 (gray dots). Results shown in Table 2 indicate that the 2.3x steeper slope ( $\Delta I_C / \Delta t_{\text{retention}}$ ) under 4%  $t_F$  variation compare to 9% counterpart offers smaller  $\Delta$  increase (82 rather than 87), requiring a 0.6x smaller  $I_C$  increase to make all of random samples have a longer retention time than 10 years.

In conclusion, we quantify the impact of  $t_F$  variation on  $\Delta$  and  $I_C$  variability in PMTJ. The  $\Delta$  variability shows considerable  $t_F$  variation dependency compared to  $I_C$  variability counterpart, offering smaller increase of  $\Delta$  and  $I_C$  as  $t_F$  variation is improved to make all of random MTJ samples meet a retention time specification.

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**References:** [1] S. Wolf, et al., *Proc. IEEE*, 2010, pp. 2155-2168. [2] K. Lee, et al., *Trans. Magn.*, 2011, pp. 131-136. [3] S. Ikeda, et al., *Nature Mater.*, 2011, pp. 721-724. [4] H. Sato, et al., *APL*, 2011, pp. 042501. [5] K. Tsunoda, et al., *IEDM*, 2014. [6] J. Hayakawa, et al., *Jpn. JAP*, 2005, pp. L587-L589. [7] J. Kim, et al., *DRC*, 2014. [8] K.C. Chun, et al., *JSSC*, 2013, pp. 2240-2243. [9] H. Zhao, et al., *JAP*, 2011, pp. 07C720. [10] K. Hofmann, et al., *VLSI Tech. Symp.* 2014.



$$\Delta = \frac{H_k \cdot M_s \cdot V}{2k_B T} \quad H_{k\perp} = \frac{K_i}{t_F} - 4\pi \cdot N_{dz} \cdot M_s$$

$$I_C = \frac{2e \cdot \alpha \cdot M_s (H_{k\perp} - 4\pi \cdot N_{dz} \cdot M_s) \cdot V}{\hbar \cdot \eta}$$

● : a function of PMTJ dimensions

Fig. 1. The anisotropy field ( $H_k$ ), thermal stability factor ( $\Delta$ ), and switching current ( $I_C$ ) in interface perpendicular magnetic tunnel junction (PMTJ) show a strong dependency of process-dependent dimensional variations.

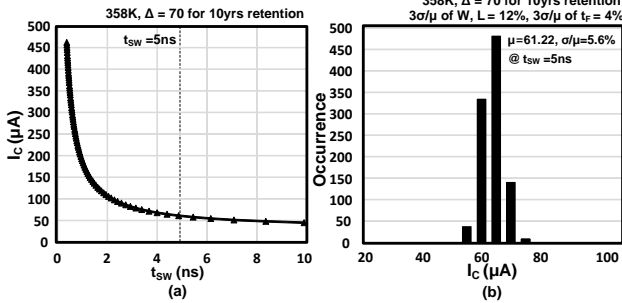


Fig. 2. (a)  $I_C$  as a function of  $t_{sw}$  and (b)  $I_C$  variation under free layer  $W, L$  variation of 12% and  $t_F$  variation of 4% ( $t_{sw}=5ns$ ).

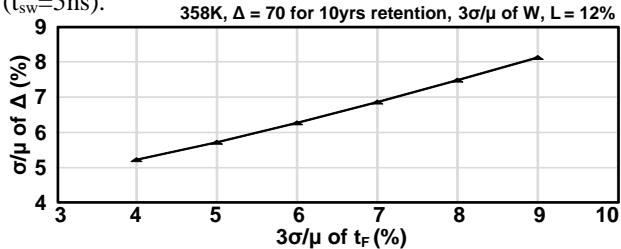


Fig. 4. The  $\Delta$  variability has a strong dependency on  $t_F$  variation.

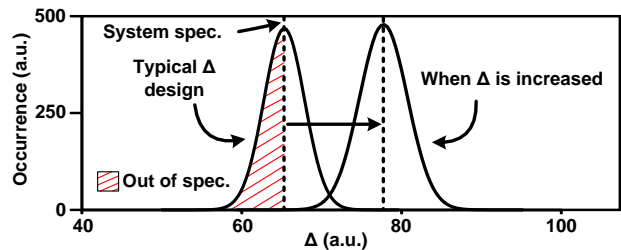


Fig. 6. Increasing  $\Delta$  would be considered to make all of random samples meet a target of 10 years retention [10].

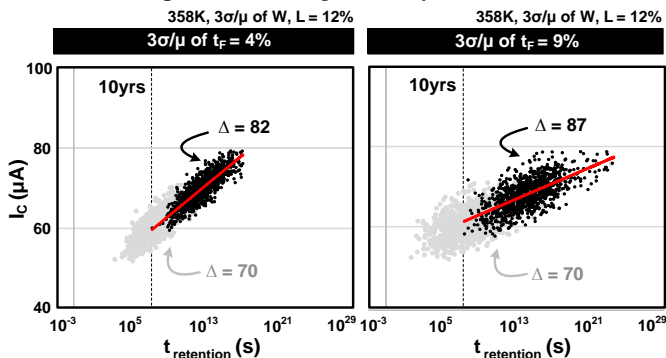


Fig. 7. Replotted correlation maps after increasing  $\Delta$ .

64MB L3 cache memory,  $\Delta = 70$  for 10yrs retention

Quantity	PMTJ [3], [5], [6]
Anisotropy source	Interface
Sat. Magnetization, $M_s$ ( $10^3 A/m$ )	1077
Polarization factor, $P$	0.6
Effective critical thickness, $t_c$ (nm)	3 (1.5 x 2, double MgO interface*)
Gilbert Damping, $\alpha$	$t_F$ dependent**
Length, width of free layer, $L, W$ (nm)	$\mu=22, \mu=22$ ( $3\sigma/\mu=12\%^{***}$ )
Thickness of free layer, $t_F$ (nm)	$\mu=2.78$ ( $3\sigma/\mu=4^{***-9\%}$ )

\* To increase the  $\Delta$  for 10yrs retention, double MgO interface is used [5]

\*\*  $t_F$  dependent  $\alpha$  is used [3], \*\*\* ITRS roadmap

Table 1. Variation factors and realistic PMTJ material parameters used in the variability analysis.

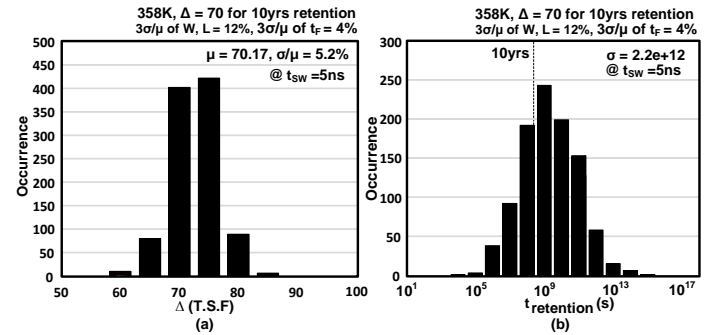


Fig. 3. Variation of (a)  $\Delta$  and (b)  $t_{retention}$  under free layer  $W, L$  variation of 12% and  $t_F$  variation of 4%.

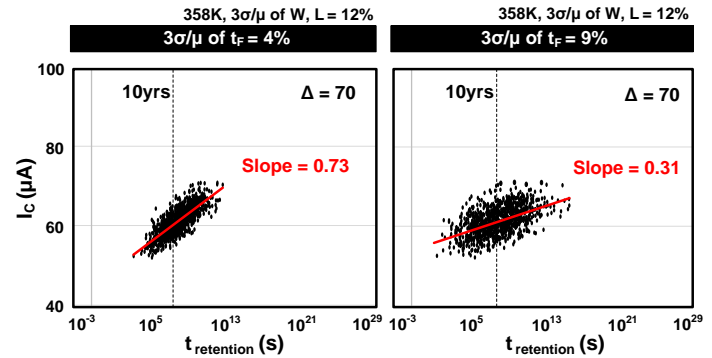


Fig. 5. Correlation maps between  $t_{retention}$  and  $I_C$  variability under different  $t_F$  variation conditions (4%, 9%). A slope ( $\Delta I_C / \Delta t_{retention}$ ) difference suggests that the  $t_{retention}$  variability has a stronger dependency on  $t_F$  variation compared to  $I_C$  variability counterpart.

Quantity		3σ/μ of $t_F = 4\%$		3σ/μ of $t_F = 9\%$	
Typical $\Delta$ design	$\Delta$ for 10yrs $t_{retention}$	70		70	
	$I_C$ ( $\mu A$ )	Avg.	$\sigma/\mu$	Avg.	$\sigma/\mu$
	$\Delta$	70.17	5.2%	70.27	8.1%
	$\Delta I_C / \Delta t_{retention}$ ( $\mu A/s$ )	0.73 (2.3x)		0.31 (1x)	
When $\Delta$ is increased	$\Delta$ for $t_{retention, Min} > 10yrs$	82		87	
	$I_C$ ( $\mu A$ )	Avg.	$\sigma/\mu$	Avg.	$\sigma/\mu$
Remark (required $I_C$ for increasing $\Delta$ )		6.89μA (0.6x)		10.72μA (1x)	

Table 2. The 2.3x steeper slope ( $\Delta I_C / \Delta t_{retention}$ ) under 4%  $t_F$  variation compared to 9% counterpart offers smaller  $\Delta$  increase (82 rather than 87), requiring a 0.6x smaller  $I_C$  increase to make all of random samples have a longer retention time than 10 years.