Due Friday 09/13/13 (5pm; Xiaofan's office, Keller Hall 5-149)

- 1. Problem 2.2 from the book (page 20; attached).
- 2. Consider the unforced mass-spring system

$$m\ddot{y} + g(y) = 0$$

with three different models for the spring force

- hardening spring:  $g(y) = k(1 + y^2)y;$
- softening spring:  $g(y) = k(1 y^2)y;$
- linear spring: g(y) = k y,

and k > 0.

- (a) Determine a state-space representation of this system.
- (b) Find equilibrium points of the above systems. Discuss your observations for three different spring force models.
- (c) Is this system
  - causal,
  - time-varying,
  - linear,
  - memoryless,
  - finite-dimensional?

Explain.

- (d) For three different spring force models with m = k = 1, use Matlab to simulate systems' responses from different initial conditions. Plot corresponding results in the phase plane (horizontal axis determined by position y(t), vertical axis determined by velocity  $\dot{y}(t)$ ) and discuss your observations.
- 3. The system shown in Figure 1 is composed of a first order system followed by a saturation element. Which of the following properties does this system have a) causality, b) linearity c) time-invariance? Is the system memoryless? Compute the output y that corresponds to the periodic input in Figure 1.

**Note:** The saturation function works as follows: if the two signals g and y are related by y(t) = Saturation (g(t)), then

$$y(t) = \begin{cases} g(t) & \text{if } |g(t)| \leq 1 \\ 1 & \text{if } g(t) > 1 \\ -1 & \text{if } g(t) < -1 \end{cases}$$



Figure 1: System in Problem 3.

Does such an equilibrium point always exist?

(d) Assume that b = 1/2 and  $mg\ell = 1/4$ . Compute the torque T(t) needed for the pendulum to fall from  $\theta(0) = 0$  with constant velocity  $\dot{\theta}(t) = 1$ ,  $\forall t \ge 0$ . Linearize the system around this trajectory.

**2.2 (Local linearization around a trajectory).** A single-wheel cart (unicycle) moving on the plane with linear velocity v and angular velocity  $\omega$  can be modeled by the nonlinear system

$$\dot{p}_x = v \cos \theta, \qquad \dot{p}_y = v \sin \theta, \qquad \dot{\theta} = \omega, \qquad (2.11)$$

where  $(p_x, p_y)$  denote the Cartesian coordinates of the wheel and  $\theta$  its orientation. Regard this as a system with input  $u := \begin{bmatrix} v & \omega \end{bmatrix}' \in \mathbb{R}^2$ .

(a) Construct a state-space model for this system with state

$$x = \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} := \begin{bmatrix} p_x \cos \theta + (p_y - 1) \sin \theta \\ -p_x \sin \theta + (p_y - 1) \cos \theta \\ \theta \end{bmatrix}$$

and output  $y := \begin{bmatrix} x_1 & x_2 \end{bmatrix}' \in \mathbb{R}^2$ .

- (b) Compute a local linearization for this system around the equilibrium point  $x^{eq} = 0$ ,  $u^{eq} = 0$ .
- (c) Show that  $\omega(t) = v(t) = 1$ ,  $p_x(t) = \sin t$ ,  $p_y(t) = 1 \cos t$ ,  $\theta(t) = t$ ,  $\forall t \ge 0$  is a solution to the system.
- (d) Show that a local linearization of the system around this trajectory results in an LTI system.

**2.3 (Feedback linearization controller).** Consider the inverted pendulum in Figure 2.6.

(a) Assume that you can directly control the system in torque, i.e., that the control input is u = T.

Design a feedback linearization controller to drive the pendulum to the upright position. Use the following values for the parameters:  $\ell = 1 \text{ m}$ , m = 1 kg,  $b = 0.1 \text{ N m}^{-1} \text{ s}^{-1}$ , and  $g = 9.8 \text{ m s}^{-2}$ . Verify the performance of your system in the presence of measurement noise using Simulink<sup>®</sup>.

(b) Assume now that the pendulum is mounted on a cart and that you can control the cart's jerk, which is the derivative of its acceleration *a*. In this case,

$$T = -m\,\ell\,a\cos\theta, \qquad \dot{a} = u.$$

Design a feedback linearization controller for the new system.

What happens around  $\theta = \pm \pi/2$ ?

Note that, unfortunately, the pendulum needs to pass by one of these points for a swing-up, i.e., the motion from  $\theta = \pi$  (pendulum down) to  $\theta = 0$  (pendulum upright).

Attention! Writing the system in the carefully chosen coordinates  $x_1$ ,  $x_2$ ,  $x_3$ is crucial to getting an LTI linearization. If one tried to linearize this system in the original coordinates  $p_x$ ,  $p_y$ ,  $\theta$  with dynamics given by (2.11), one would get an LTV system.