

# LINEAR CONTROL SYSTEMS: WEEK 1.

Note Title

9/9/2009

## MODELING:

The primary modeling methodologies are

- ① Physical modelling
- ② Input-output based black-box modeling

In many practical scenarios a mix of physical and black-box modeling techniques are employed.

We will first present examples of physical modeling; followed by black-box modeling techniques; followed by the relationships of the two modeling methodologies.

## Physical modeling:

- Use of physics based laws to obtain mathematical descriptions of the system under study

## Mechanical Systems

→ Mostly governed by Newton's laws of motion particularly the last two laws.

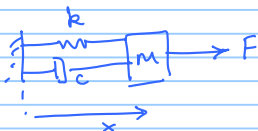
→ Consider any body with mass 'm' that is acted upon by a net force  $\vec{F}$ .

Then 
$$\vec{F} = m\vec{a}$$

where  $\vec{a}$  is the acceleration of the body  $m$  (2<sup>nd</sup> law)

→ Every action has an equal and opposite reaction. (Third law)

Example 1:



→ A linear (Hookean) spring exerts a force  $kx$  in the direction opposite to the direction of the displacement  $x$ .

→ A viscous damper exerts a force  $c\dot{x}$  in the direction opposite to the displacement  $x$ .

Free-body diagram:



Net force on the mass  $m$  in the direction of motion is

$$f_{\text{net}} = F - kx - c\dot{x}$$

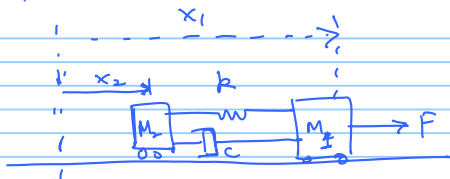
∴ from Newton's laws

$$m \frac{d^2x}{dt^2} = F - kx - c\dot{x}$$

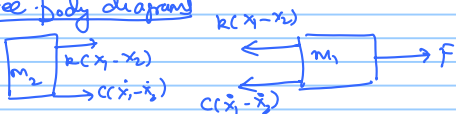
$$\Rightarrow \boxed{m \frac{d^2x}{dt^2} + c\dot{x} + kx = F.}$$

The above differential equation is the mathematical description of a spring-mass-damper system.

## Example 2



Free body diagrams



Net force acting on mass  $m_1$  is

$$F - k(x_1 - x_2) - c(\dot{x}_1 - \dot{x}_2)$$

$\therefore$

$$m_1 \frac{d^2 x_1}{dt^2} = F - k(x_1 - x_2) - c(\dot{x}_1 - \dot{x}_2)$$

$$\Rightarrow m_1 \frac{d^2 x_1}{dt^2} + c\dot{x}_1 - c\dot{x}_2 + kx_1 - kx_2 = F$$

Net force acting on mass  $m_2$  is

$$k(x_1 - x_2) + c(\dot{x}_1 - \dot{x}_2)$$

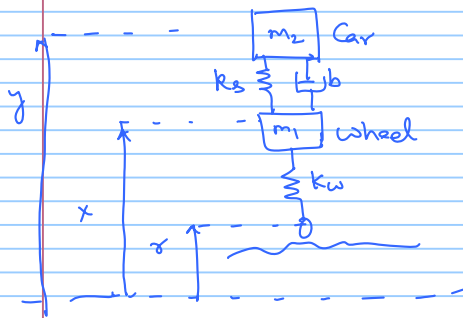
$$\therefore m_2 \frac{d^2 x_2}{dt^2} = k(x_1 - x_2) + c(\dot{x}_1 - \dot{x}_2)$$

$$\Rightarrow m_2 \frac{d^2 x_2}{dt^2} - c\dot{x}_1 + c\dot{x}_2 - kx_1 + kx_2 = 0$$

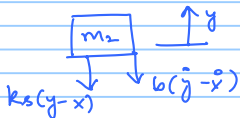
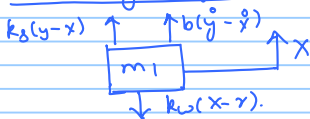
∴ The mathematical model describing the two mass system is

$$\begin{aligned}
 m_1 \frac{d^2 x_1}{dt^2} + c \dot{x}_1 - \dot{x}_2 + kx_1 - kx_2 &= F \\
 m_2 \frac{d^2 x_2}{dt^2} - c \dot{x}_1 + \dot{x}_2 - kx_1 + kx_2 &= 0
 \end{aligned}$$

Example 3: A quarter Car model:



Free body diagrams:



Net force on  $m_1$  in the direction of  $x$  is

$$k_s(y-x) + b(\dot{y}-\dot{x}) - k_w(x-r)$$

$$\therefore m_1 \frac{d^2x}{dt^2} = k_s(y-x) + b(\dot{y}-\dot{x}) - k_w(x-r)$$

$$\Rightarrow m_1 \frac{d^2x}{dt^2} + b\dot{x} - b\dot{y} + k_sx - k_sy + k_wx = k_w r$$

Net force on the car in the direction  $y$  is

$$-k_s(y-x) - b(\dot{y}-\dot{x})$$

$$\therefore m_2 \frac{d^2y}{dt^2} = -k_s(y-x) - b(\dot{y}-\dot{x})$$

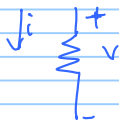
Thus, the mathematical description of the quarter car model is

$$\left\{ \begin{array}{l} m_1 \frac{d^2x}{dt^2} + b\dot{x} - b\dot{y} + k_sx - k_sy + k_wx = k_w r \\ m_2 \frac{d^2y}{dt^2} + k_s(y-x) + b(\dot{y}-\dot{x}) = 0 \end{array} \right.$$

The above are examples of translational motion. We will provide examples of rotational motion later.

# Electrical Systems

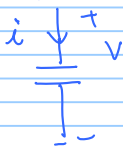
resistor:



$$V = iR$$

"The voltage drop along the direction of the current is  $iR$ . where  $R$  is the resistance"

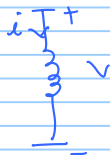
Capacitor



$$i = C \frac{dv}{dt}$$

where  $V$  is the voltage drop in the direction of the current

inductor



$$V = L \frac{di}{dt}$$

where  $V$  is the voltage drop in the direction of the current.

Two laws:

Kirchoffs Current Law (KCL)

The algebraic sum of currents at a

node is zero.

we will adopt a convention that with

respect to a node, a current leaving the

node is positive and a current entering the

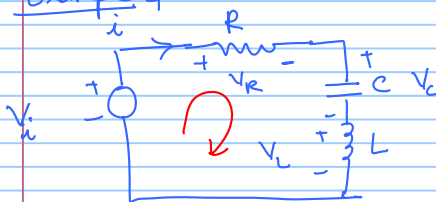
node is negative

## Kirchoff's Voltage law (KVL):

The algebraic sum of all voltages taken around a closed path is zero.

→ we will adopt the convention that a voltage drop along the path being traversed is positive and a voltage rise is negative.

Example 4:



Applying KVL we obtain

$$-V_i + V_R + V_C + V_L = 0$$

with

$$V_R = iR$$

$$C \frac{dV_C}{dt} = i$$

$$L \frac{di}{dt} = V_L$$

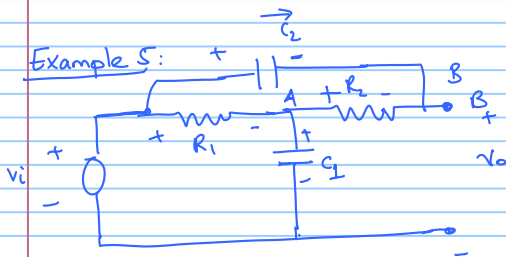


$$\Rightarrow V_R = RC \frac{dV_C}{dt}$$

$$V_L = L \frac{di}{dt} = LC \frac{d^2 V_C}{dt^2}$$

$$\therefore -V_i + RC \frac{dV_C}{dt} + V_C + LC \frac{d^2 V_C}{dt^2} = 0$$

$$\Rightarrow \boxed{LC \frac{d^2 V_C}{dt^2} + RC \frac{dV_C}{dt} + V_C = V_i}$$



Node A:

$$-\left(\frac{V_i - V_A}{R_1}\right) - \frac{V_B - V_A}{R_2} + C_1 \frac{dV_A}{dt} = 0$$

Node B:

$$+\frac{V_B - V_A}{R_2} - C_2 \frac{d(V_i - V_B)}{dt} = 0$$

$$\text{Let } V_{C_1} = V_A; \quad V_{C_2} = V_i - V_B.$$

$$V_B = V_i - V_{C_2}$$

$$\begin{aligned}
 \Rightarrow C_1 \frac{dV_{c1}}{dt} &= \frac{V_i - V_A}{R_1} + \frac{V_B - V_A}{R_2} \\
 &= \frac{V_i - V_{c1}}{R_1} + \frac{V_i - V_{c2} - V_{c1}}{R_2} \\
 &= \frac{V_i}{R_1} + \frac{V_i}{R_2} - \frac{V_{c1}}{R_1} - \frac{V_{c1}}{R_2} - \frac{V_{c2}}{R_2} \\
 &= V_i \left( \frac{1}{R_1} + \frac{1}{R_2} \right) - V_{c1} \left( \frac{1}{R_1} + \frac{1}{R_2} \right) - \frac{V_{c2}}{R_2}
 \end{aligned}$$

$$\therefore \frac{dV_{c1}}{dt} = \frac{1}{C_1} \left( \frac{1}{R_1} + \frac{1}{R_2} \right) V_i - \frac{1}{C_1} \left( \frac{1}{R_1} + \frac{1}{R_2} \right) V_{c1} - \frac{V_{c2}}{R_2}$$

Similarly

$$\frac{dV_{c2}}{dt} = -\frac{1}{C_2 R_2} V_{c1} - \frac{1}{C_2 R_2} V_{c2} + \frac{1}{C_2 R_2} V_i$$

## Rotational dynamics:

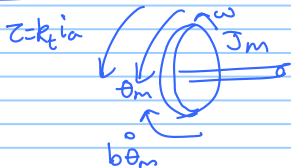
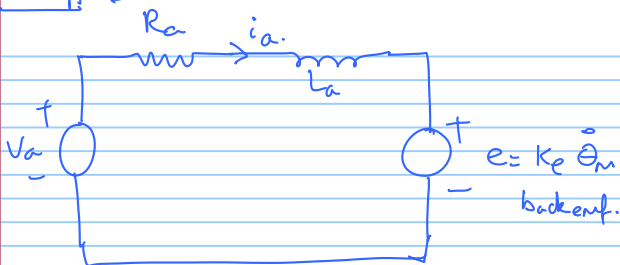
$I$   $\equiv$  moment of Inertia

$\theta$   $\equiv$  angular position

The main law is  $I \frac{d^2 \theta}{dt^2} = \tau$

where  $\tau$  is the net torque acting

Example 6:



$$-V_a + iR_a + L_a \frac{di}{dt} + k_e \dot{\theta}_m = 0$$

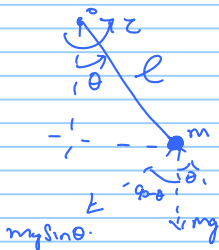
and

$$J_m \ddot{\theta}_m = k_t i_a - b \dot{\theta}_m + \tau$$

$$\therefore \boxed{J_m \ddot{\theta}_m + b \dot{\theta}_m = k_t i_a + \tau} \quad \text{--- (1)}$$

$$k_e \dot{\theta}_m + L_a \frac{di_a}{dt} + R_a i_a = V_a \quad \text{--- (2)}$$

## Example 7



applied torque =  $\tau$

restoring moment =  $-(mg \sin \theta) l$

Net torque =  $\tau - mg l \sin \theta$

$$\therefore I \ddot{\theta} = \tau - mg l \sin \theta$$

$$I \ddot{\theta} + mg l \sin \theta = \tau$$

$$\Rightarrow m l^2 \ddot{\theta} = \tau - mg l \sin \theta$$

$$\Rightarrow \boxed{\ddot{\theta} + \frac{g}{l} \sin \theta = \frac{\tau}{m l^2}}$$

Thus, we have seen that many systems admit mathematical descriptions that are ordinary differential equations