

Design of structured optimal feedback gains for interconnected systems

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joint work with:

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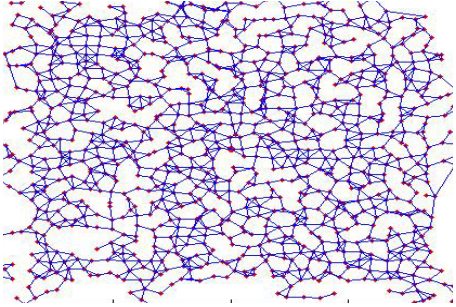
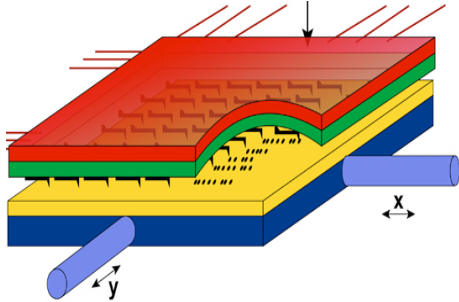
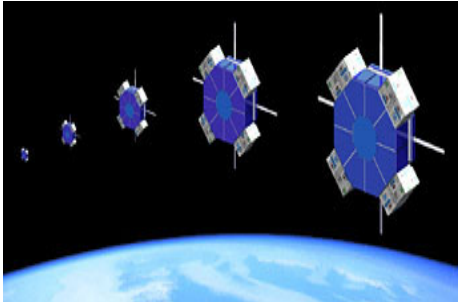


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Distributed systems

- OF INCREASING IMPORTANCE IN MODERN TECHNOLOGY

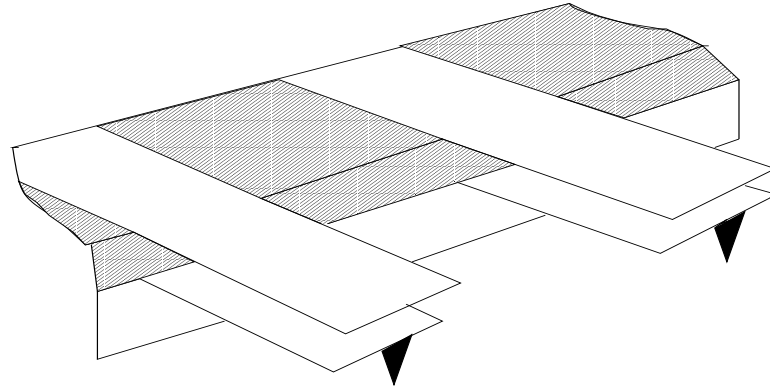
APPLICATIONS:

sensor networks	arrays of micro-cantilevers	UAV formations satellite constellations
		

- INTERACTIONS CAUSE COMPLEX BEHAVIOR
cannot be predicted by analyzing isolated subsystems
- SPECIAL STRUCTURE
every unit has sensors and actuators

Array of micro-cantilevers

ELECTROSTATICALLY ACTUATED MICRO-CANTILEVERS



POTENTIAL APPLICATION: **MASSIVELY PARALLEL DATA STORAGE**

problem: **slow scans** \equiv **low throughput**

solution: **go massively parallel**

ISSUES:

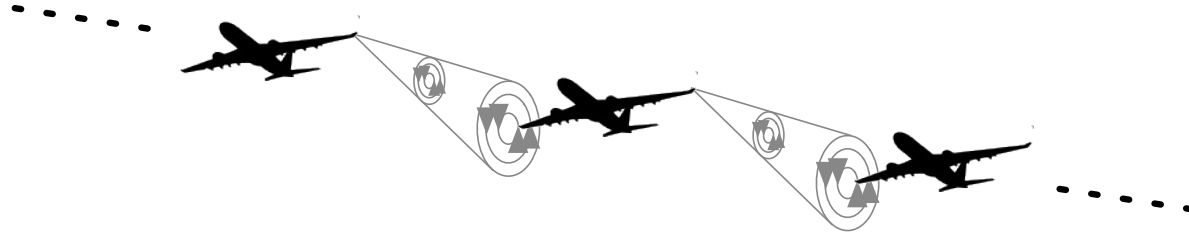
tightly coupled dynamics \Rightarrow **spatio-temporal instabilities**

large number of devices \Rightarrow **localized control imperative**

Coordinated control of formations

FORMATION FLIGHT FOR AERODYNAMIC ADVANTAGE

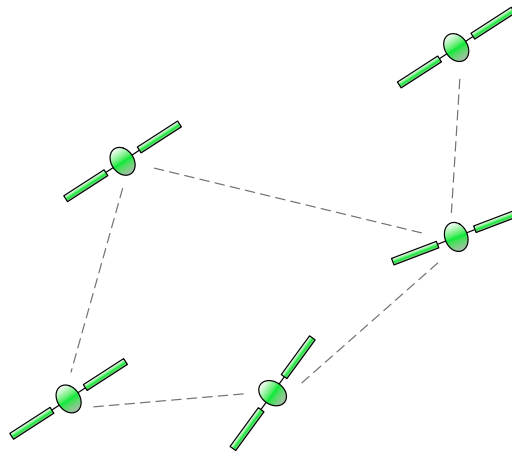
e.g. additional lift in V-formations



precise control needed

MICRO-SATELLITE FORMATIONS

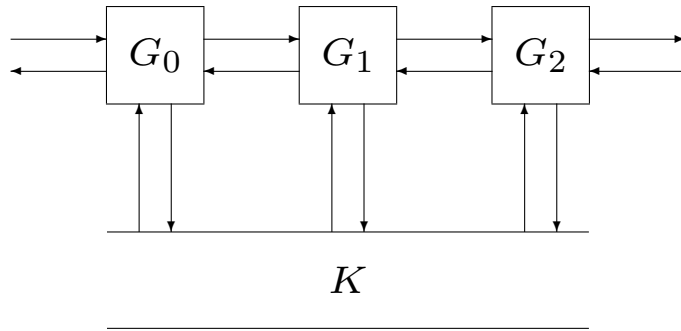
e.g. for synthetic aperture



MAKE VEHICLES SMALLER AND CHEAPER \Rightarrow USE MANY
cooperative control becomes a major issue

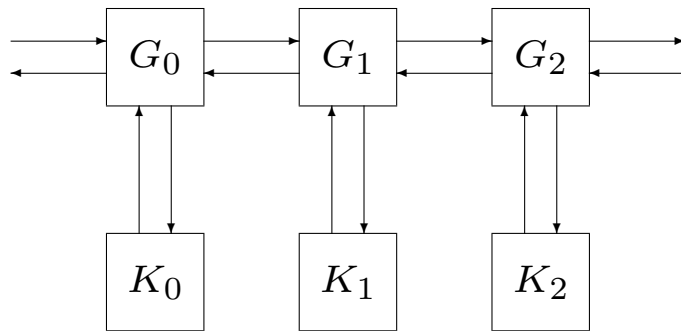
Controller architectures

CENTRALIZED



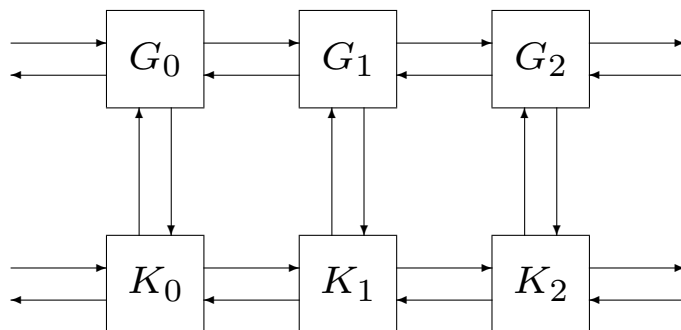
best performance
excessive communication

FULLY DECENTRALIZED



worst performance
no communication

LOCALIZED



many possible architectures

Outline

① STRUCTURED OPTIMAL DESIGN

- ★ sparsity constraints on feedback gains

② OPTIMAL LOCALIZED CONTROL OF VEHICULAR PLATOONS

- ★ design of spatially-varying feedback gains

③ PERFORMANCE VS. SIZE

- ★ coherence of formation

④ PARTING THOUGHTS

STRUCTURED OPTIMAL DESIGN

Structured H_2 problem

$$\begin{aligned} \dot{x} &= Ax + B_1 d + B_2 u \\ z &= \begin{bmatrix} Q^{1/2} \\ 0 \end{bmatrix} x + \begin{bmatrix} 0 \\ R^{1/2} \end{bmatrix} u \\ u &= -Kx \end{aligned} \quad K \in \mathcal{S}$$

- STRUCTURAL CONSTRAINTS $K \in \mathcal{S}$

centralized

$$\begin{bmatrix} * & * & * & * \\ * & * & * & * \\ * & * & * & * \\ * & * & * & * \end{bmatrix}$$

fully decentralized

$$\begin{bmatrix} \diamond & & & \\ & * & & \\ & & \triangle & \\ & & & * \end{bmatrix}$$

localized

$$\begin{bmatrix} * & * & & \\ * & * & * & \\ & * & * & * \\ & & * & * \end{bmatrix}$$

OBJECTIVE:

design stabilizing $K \in \mathcal{S}$ that minimizes $\|d \rightarrow z\|_2^2$

- CLOSED-LOOP SYSTEM

$$\begin{aligned}\dot{x} &= (A - B_2 K) x + B_1 d \\ z &= \begin{bmatrix} Q^{1/2} \\ -R^{1/2} K \end{bmatrix} x, \quad K \in \mathcal{S}\end{aligned}$$

STRUCTURED H_2 PROBLEM:

<p>minimize $J(K) := \text{trace}(P(K)B_1B_1^T)$</p> <p>subject to $\begin{cases} (A - B_2K)^T P + P(A - B_2K) = -(Q + K^T R K) \\ K \in \mathcal{S} \end{cases}$</p>

$J(K)$ – nonconvex function of K

- RELATED PROBLEMS:

- ★ **static output feedback:** Levine & Athans, IEEE TAC'70
- ★ **structured dynamic controller:** Wenk & Knapp, IEEE TAC'80

Necessary conditions for optimality

$$\begin{aligned}
 (A - B_2 K)^T P + P (A - B_2 K) &= -(Q + K^T R K) \\
 (A - B_2 K) L + L (A - B_2 K)^T &= -B_1 B_1^T \\
 [(R K - B_2^T P) L] \circ I_S &= 0
 \end{aligned}$$

I_S - structural identity

$$K = \begin{bmatrix} * & * & & & \\ * & * & * & & \\ & * & * & * & \\ & & * & * & \end{bmatrix} \Rightarrow I_S = \begin{bmatrix} 1 & 1 & & & \\ 1 & 1 & 1 & & \\ & 1 & 1 & 1 & \\ & & 1 & 1 & \end{bmatrix}$$

- SPECIAL CASES:

- ★ no constraints

$$A^T P + P A - P B_2 R^{-1} B_2^T P + Q = 0$$

$$K_c = R^{-1} B_2^T P$$

- ★ expensive control of stable open-loop systems

perturbation analysis: Fardad, Lin, Jovanović, CDC'09

Perturbation analysis

- EXPENSIVE CONTROL: $R = (1/\varepsilon) I, \quad 0 < \varepsilon \ll 1$

$$P = \sum_{n=0}^{\infty} \varepsilon^n P_n, \quad L = \sum_{n=0}^{\infty} \varepsilon^n L_n, \quad K = \sum_{n=0}^{\infty} \varepsilon^n K_n$$

$$O(1) : \quad K_0 = 0$$

$$O(\varepsilon) : \begin{cases} A^T P_0 + P_0 A = -Q \\ A L_0 + L_0 A^T = -B_1 B_1^T \\ [K_1 L_0] \circ I_S = [B_2^T P_0 L_0] \circ I_S \end{cases}$$

$$O(\varepsilon^2) : \begin{cases} A^T P_1 + P_1 A = (\text{matrix function of } K_1 \text{ and } P_0) \\ A L_1 + L_1 A^T = (\text{matrix function of } K_1 \text{ and } L_0) \\ [K_2 L_0] \circ I_S = [B_2^T (P_0 L_1 + P_1 L_0) - K_1 L_1] \circ I_S \end{cases}$$

followed by homotopy

Numerical computation

$$\begin{aligned} (A - B_2 K)^T P + P (A - B_2 K) &= -(Q + K^T R K) \\ (A - B_2 K) L + L (A - B_2 K)^T &= -B_1 B_1^T \\ [(R K - B_2^T P) L] \circ I_S &= 0 \end{aligned}$$

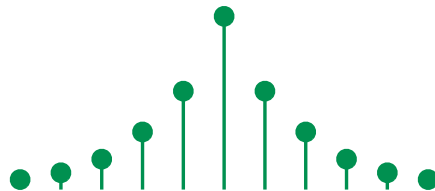
• NEWTON'S METHOD

$$K_{i+1} = K_i + s_i \tilde{K}_i \text{ until } \|\nabla J(K_i)\| < \text{tolerance}$$

• FEATURES:

- ★ Newton direction \tilde{K}_i : conjugate-gradient method
sparsity utilized
- ★ step size s_i : backtracking line search
stability guaranteed
- ★ initial condition: truncated centralized gain $K_c \circ I_S$
exponential decay

Bamieh, Paganini, Dahleh, IEEE TAC'02; Motee & Jadbabaie, IEEE TAC'08



Augmented Lagrangian

$$K = \begin{bmatrix} k_{11} & 0 \\ 0 & k_{22} \end{bmatrix}$$



$$0 = k_{12} = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} k_{11} & k_{12} \\ k_{21} & k_{22} \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} = \text{trace} \left(\begin{bmatrix} 0 & 0 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} k_{11} & k_{12} \\ k_{21} & k_{22} \end{bmatrix} \right)$$



$$K \in \mathcal{S} \Leftrightarrow \text{trace}(\Lambda^T K) = 0, \quad \Lambda \in \mathcal{S}^c$$

$$K = \begin{bmatrix} \diamond & \\ & \star \end{bmatrix} \Rightarrow \Lambda = \begin{bmatrix} 0 & \lambda_1 \\ \lambda_2 & 0 \end{bmatrix}, \quad I_{\mathcal{S}}^c = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix}$$

AUGMENTED LAGRANGIAN:

$$\mathcal{L}_\gamma(K, \Lambda) = J(K) + \text{trace}(\Lambda^T K) + \gamma \|K \circ I_{\mathcal{S}}^c\|_F^2$$

Augmented Lagrangian minimization

$$\min_K \mathcal{L}_\gamma(K, \Lambda)$$

OPTIMALITY OF \mathcal{L}_γ : NECESSARY CONDITIONS

$$\begin{aligned} (A - B_2K)^T P + P(A - B_2K) &= -(Q + K^T R K) \\ (A - B_2K) L + L(A - B_2K)^T &= -B_1 B_1^T \\ 2(RK - B_2^T P) L + \Lambda + \gamma(K \circ I_S^c) &= 0 \end{aligned}$$

- NEWTON'S METHOD WITH LINE SEARCH

- ★ Stability guaranteed
- ★ Deals with ill-conditioning

- UPDATE RULES

$$\Lambda_{i+1} = \Lambda_i + \gamma_i (K_i \circ I_S^c), \quad \gamma_{i+1} = c \gamma_i, \quad c > 1$$

- STOPPING CRITERION

$$\|K_i \circ I_S^c\|_F < \text{tolerance}$$

Part 1: summary

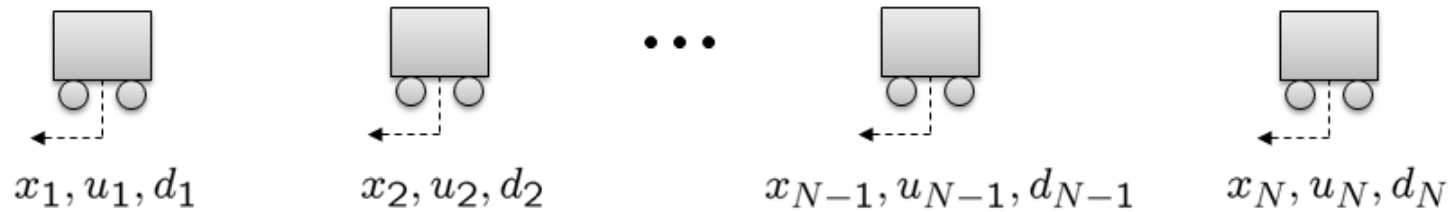
- STRUCTURED H_2 PROBLEM
 - ★ Primal formulation (perturbation analysis & homotopy)
 - ★ Augmented Lagrangian
- COMPUTATION OF OPTIMAL STRUCTURED GAINS
 - ★ Possible
- CHALLENGES
 - ★ Understand limitations of proposed methods
 - ★ Understand structure of augmented Lagrangian formulation
 - ★ Perturbation analysis/homotopy for unstable open-loop systems
 - ★ Hidden convexity?

CONTROL OF VEHICULAR FORMATIONS

Vehicular platoons

AUTOMATED CONTROL OF EACH VEHICLE

tight spacing at highway speeds



KEY ISSUES (also in: control of swarms, flocks, formation flight)

- ★ Is it enough to only look at neighbors?
- ★ How does performance scale with size?
- ★ Are there any fundamental limitations?

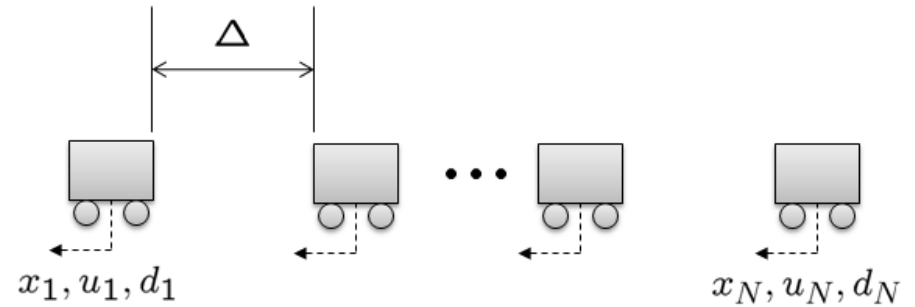
FUNDAMENTALLY DIFFICULT PROBLEM (scales badly)

Jovanović & Bamieh, IEEE TAC '05

Bamieh, Jovanović, Mitra, Patterson, IEEE TAC '10 (conditionally accepted)

Problem formulation

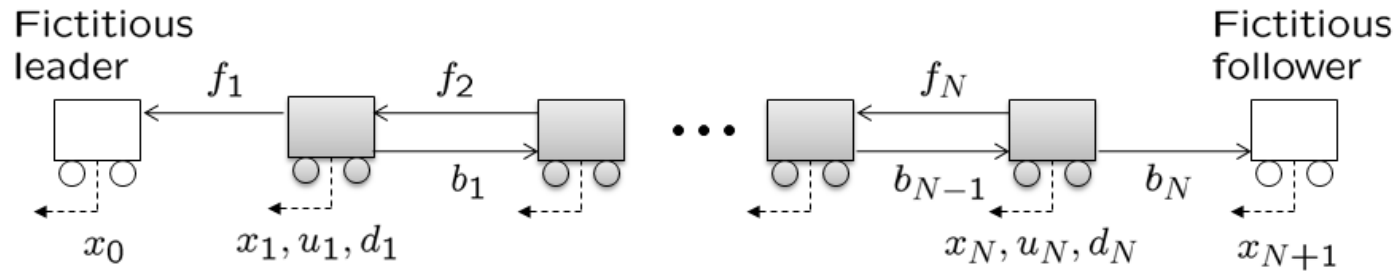
$$\dot{x}_n = \underset{\substack{\uparrow \\ \text{control}}}{u_n} + \underset{\substack{\uparrow \\ \text{disturbance}}}{d_n}$$



- DESIRED TRAJECTORY: $\left\{ \begin{array}{l} \bar{x}_n := vt + n\Delta \\ \text{constant velocity} \end{array} \right.$

- DEVIATIONS: $\left. \begin{array}{l} \tilde{x}_n := x_n - \bar{x}_n \\ \tilde{u}_n := u_n - v \end{array} \right\} \Rightarrow \dot{\tilde{x}}_n = \tilde{u}_n + d_n$

- CONTROL: $\tilde{u} = K\tilde{x}$, K : feedback gain

DESIGN K TO USE NEAREST NEIGHBOR FEEDBACK

RELATIVE POSITION FEEDBACK:

$$\tilde{u}_n = -f_n (\tilde{x}_n - \tilde{x}_{n-1}) - b_n (\tilde{x}_n - \tilde{x}_{n+1})$$

$$\tilde{u} = - \begin{bmatrix} F_f & F_b \end{bmatrix} \begin{bmatrix} C_f \\ C_b \end{bmatrix} \tilde{x}$$

$$K \sim \underbrace{\begin{bmatrix} f_1 & 0 & 0 \\ 0 & f_2 & 0 \\ 0 & 0 & f_3 \end{bmatrix}}_{F_f} \underbrace{\begin{bmatrix} 1 & 0 & 0 \\ -1 & 1 & 0 \\ 0 & -1 & 1 \end{bmatrix}}_{C_f} + \underbrace{\begin{bmatrix} b_1 & 0 & 0 \\ 0 & b_2 & 0 \\ 0 & 0 & b_3 \end{bmatrix}}_{F_b} \underbrace{\begin{bmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \\ 0 & 0 & 1 \end{bmatrix}}_{C_b}$$

Structured feedback design

$$\dot{\tilde{x}} = d + \tilde{u}$$

$$z = \begin{bmatrix} Q^{1/2} \\ 0 \end{bmatrix} \tilde{x} + \begin{bmatrix} 0 \\ I \end{bmatrix} \tilde{u}$$

$$\tilde{u} = - \begin{bmatrix} F_f & F_b \end{bmatrix} \begin{bmatrix} C_f \\ C_b \end{bmatrix} \tilde{x}, \quad F_f, F_b - \text{diagonal}$$

spatially uniform: $F_f = F_b = I$

● PERFORMANCE MEASURES

★ **MICROSCOPIC**: local position deviation $(\tilde{x}_n - \tilde{x}_{n-1})$

$$Q_l \sim \begin{bmatrix} 2 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 2 \end{bmatrix}$$

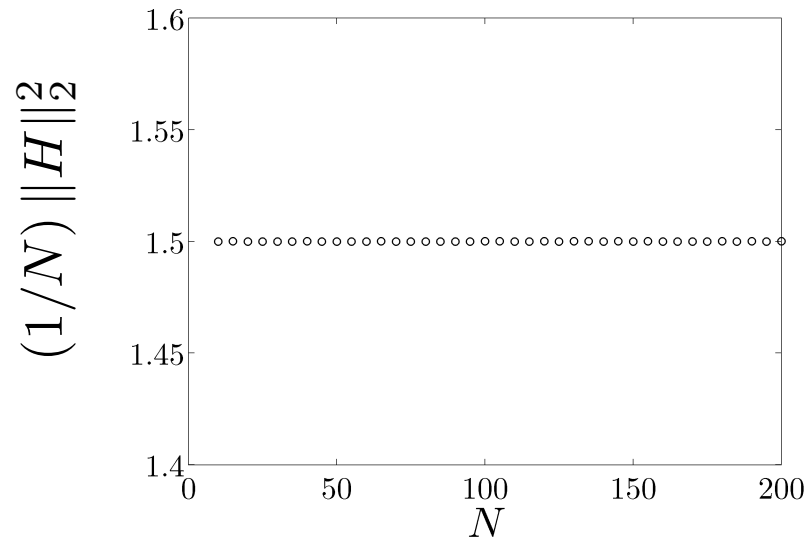
★ **MACROSCOPIC**: global position deviation \tilde{x}_n

$$Q_g = I$$

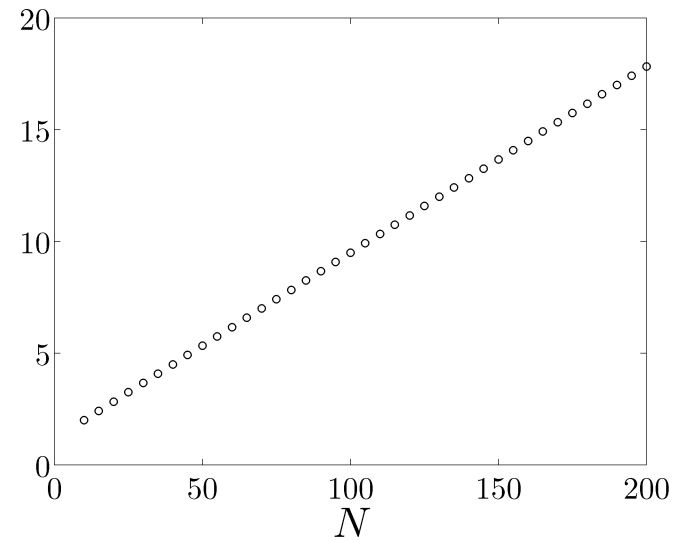
Performance vs. size

- SPATIALLY UNIFORM

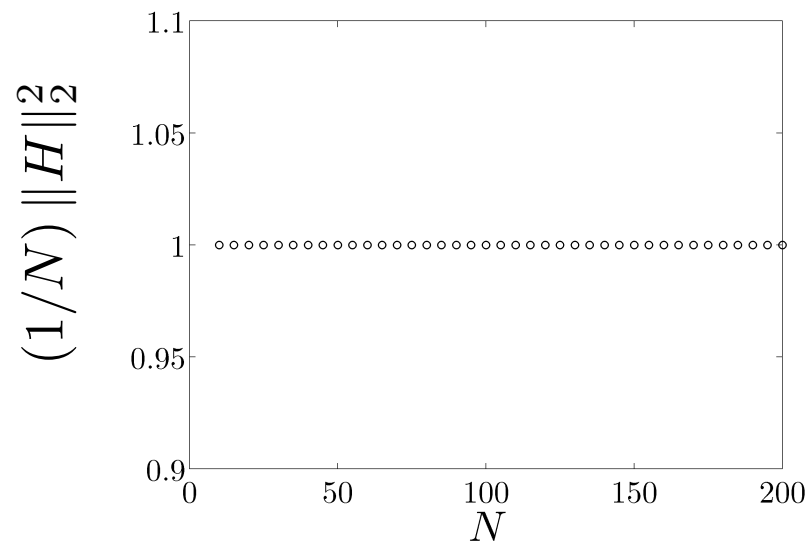
MICROSCOPIC:



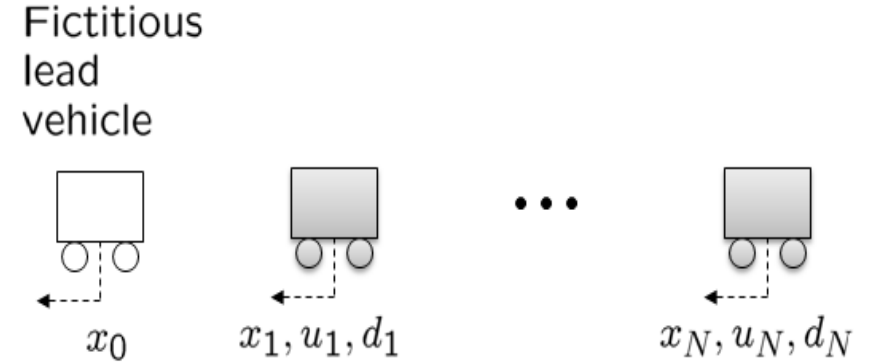
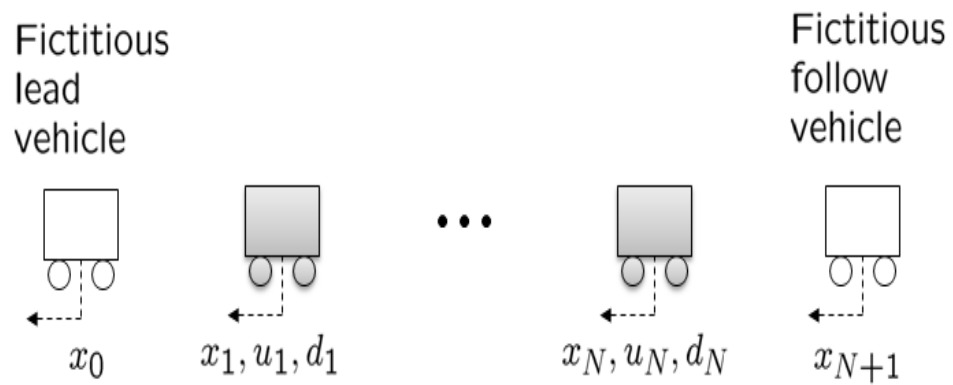
MACROSCOPIC:



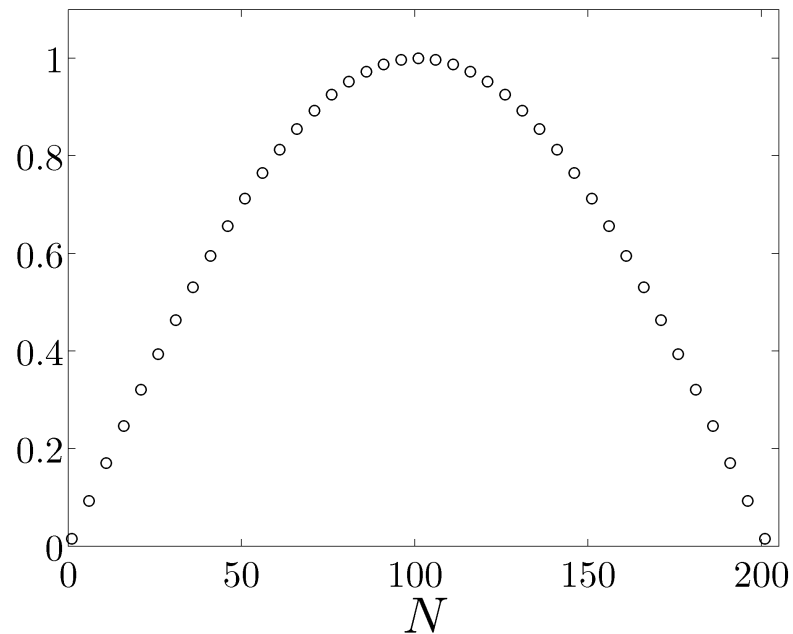
CONTROL:



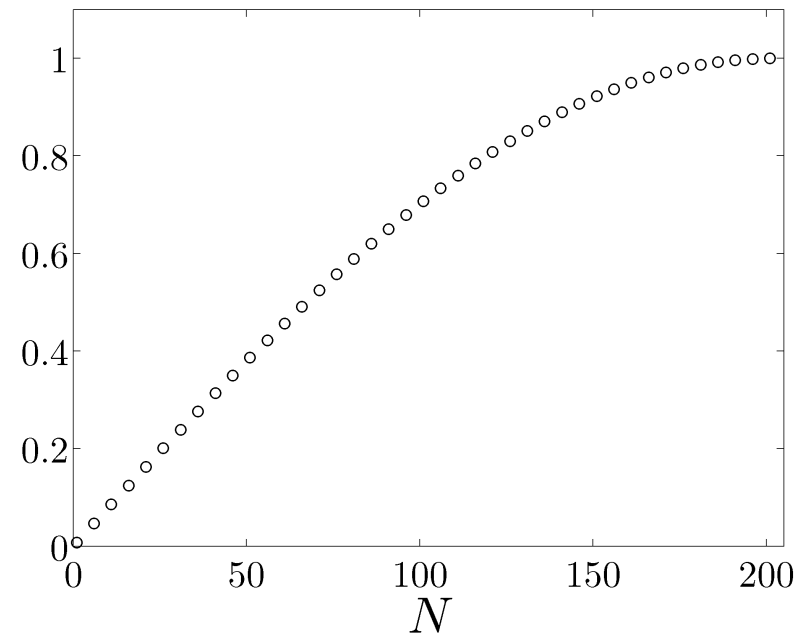
Most energetic spatial profiles



$$\sin(\pi n / (N + 1)):$$

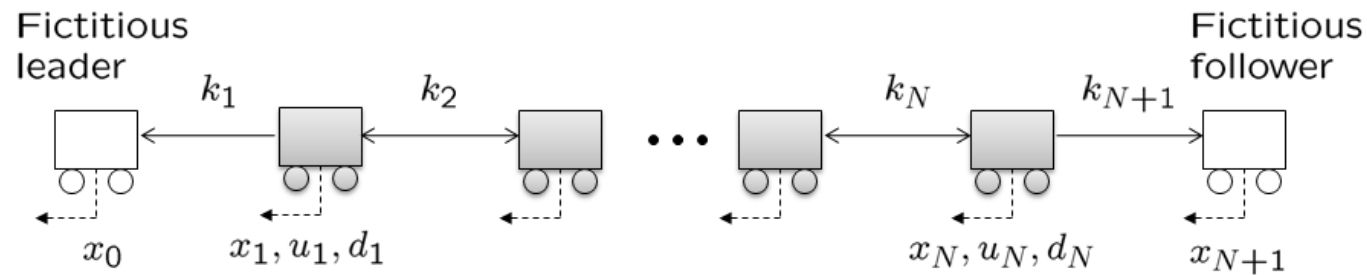


$$\cos(0.5\pi(n/(N + 1) - 1)):$$



STRUCTURED FEEDBACK DESIGN

Convex structured design



SYMMETRIC GAIN:

$$\tilde{u}_n = -k_n (\tilde{x}_n - \tilde{x}_{n-1}) - k_{n+1} (\tilde{x}_n - \tilde{x}_{n+1})$$

$$\tilde{u} = -K \tilde{x}, \quad K = K^T > 0$$

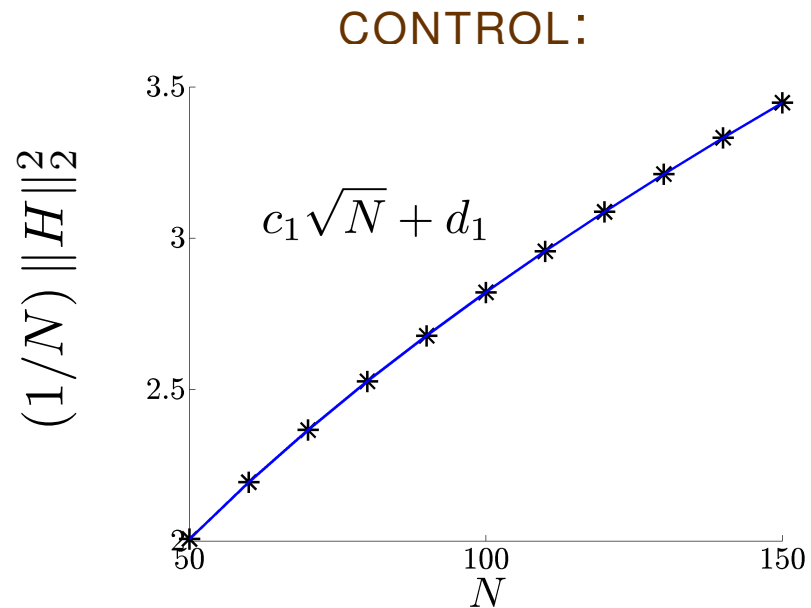
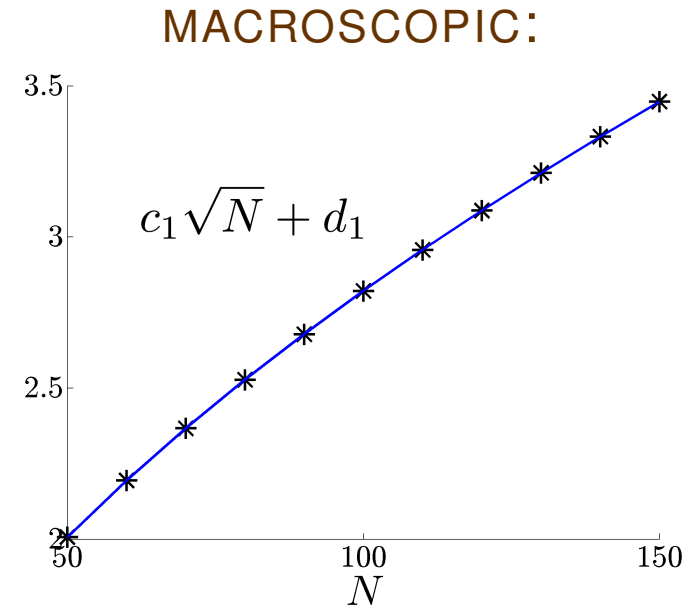
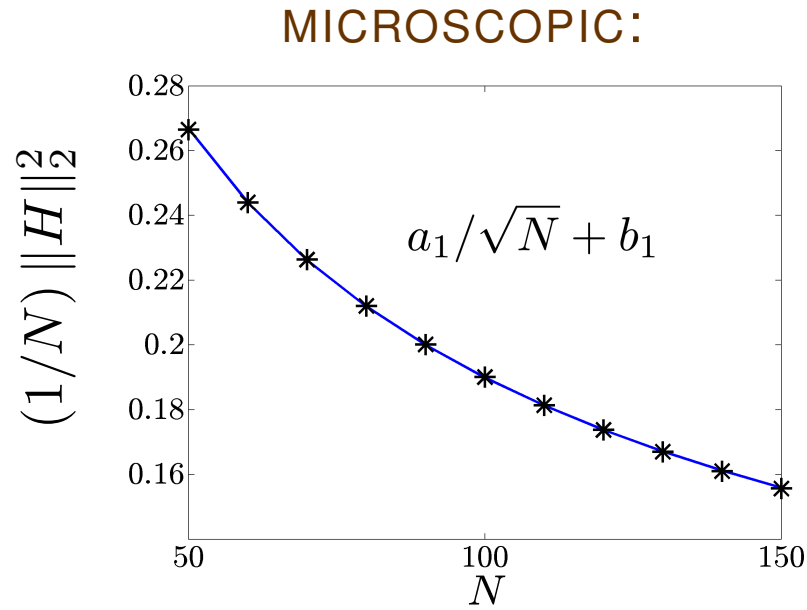
CONVEX PROBLEM:

$$\text{minimize} \quad \text{trace} (K + Q K^{-1})$$

$$\text{subject to} \quad 0 < K^T = K \in \mathcal{S}$$

Performance vs. size

- SYMMETRIC STRUCTURED OPTIMAL (WITH $Q_g = I$)



Optimal design of non-symmetric gains

- SPATIALLY UNIFORM ($K_0 = C_f + C_b$)
inversely optimal wrt $Q_0 = K_0^2$

$$\left. \begin{array}{l} -P_0^2 + Q_0 = 0 \\ K_0 = P_0 \in \mathcal{S} \end{array} \right\} \Rightarrow$$

do design with:

$$Q = Q_0 + \varepsilon(Q_d - Q_0)$$

$$P = \sum_{n=0}^{\infty} \varepsilon^n P_n, \quad L = \sum_{n=0}^{\infty} \varepsilon^n L_n, \quad K = \sum_{n=0}^{\infty} \varepsilon^n K_n$$

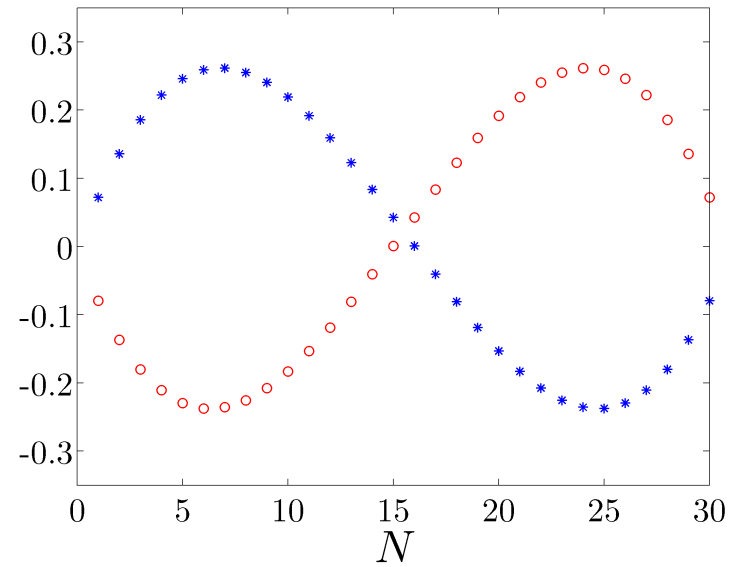
$$O(1) : \begin{cases} -P_0^2 + Q_0 = 0 \\ K_0 = P_0 \\ -K_0 L_0 - L_0 K_0 = -I \end{cases}$$

$$O(\varepsilon) : \begin{cases} -K_0 P_1 - P_1 K_0 = -(Q_d - Q_0) \\ \left[\left(\begin{bmatrix} F_{f1} & F_{b1} \end{bmatrix} \begin{bmatrix} C_f \\ C_b \end{bmatrix} - P_1 \right) L_0 \begin{bmatrix} C_f^T & C_b^T \end{bmatrix} \right] \circ \begin{bmatrix} I & I \end{bmatrix} = 0 \end{cases}$$

followed by homotopy

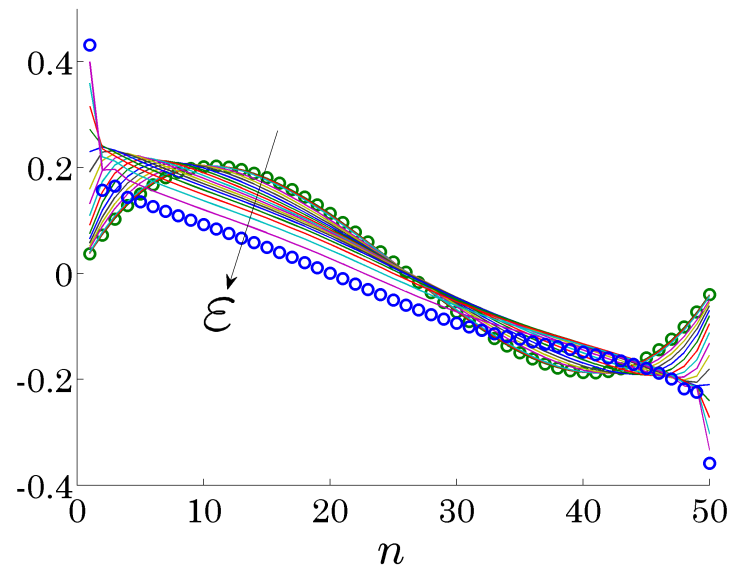
- PERTURBATION ANALYSIS (WITH $Q_g = I$)

FORWARD/BACKWARD GAINS:



- HOMOTOPY

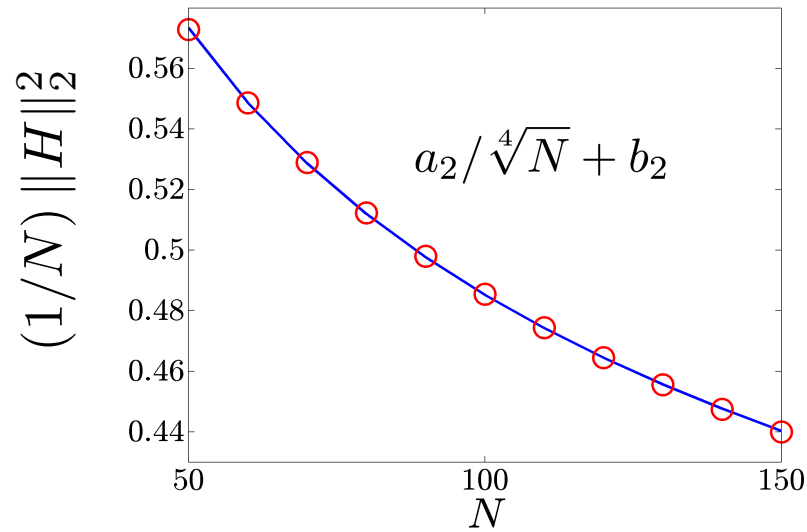
FORWARD GAINS:



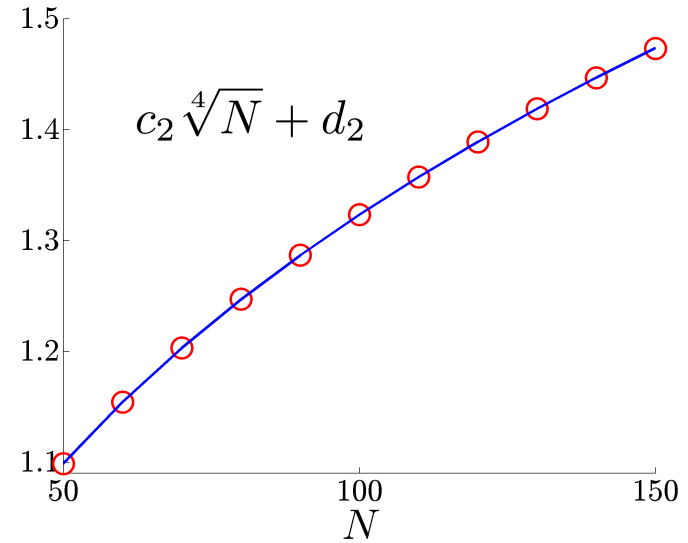
Performance vs. size

- STRUCTURED OPTIMAL (WITH $Q_d = I$)

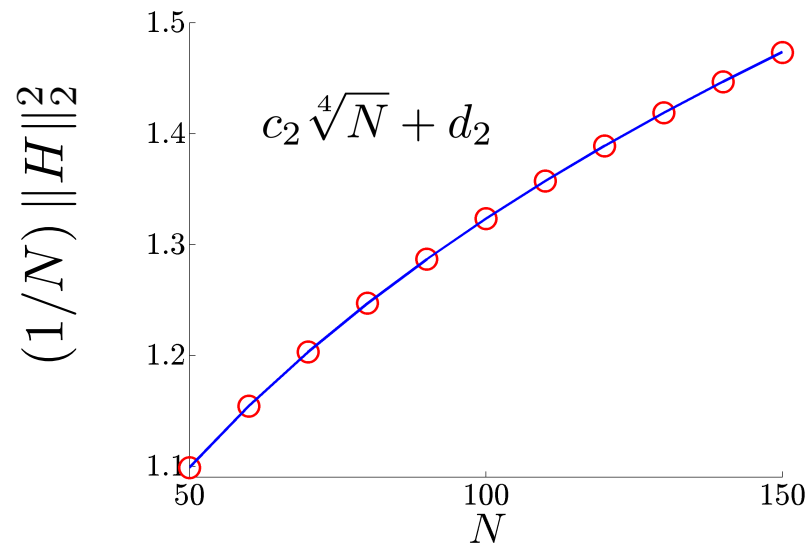
MICROSCOPIC:



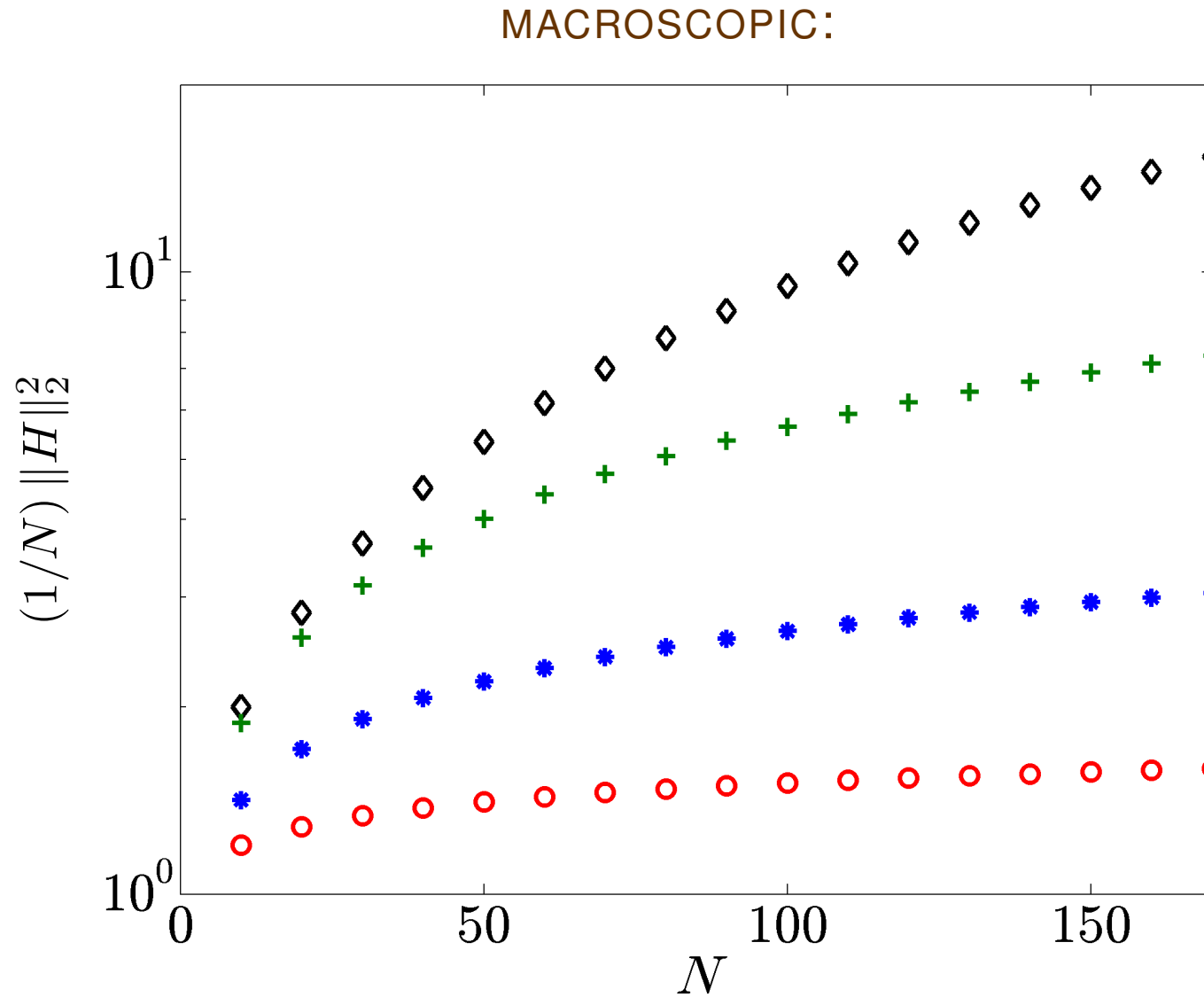
MACROSCOPIC:



CONTROL:



- **spatial uniform** vs. **symmetric structured optimal** vs. **structured optimal** vs. **centralized optimal**



Part 2: summary

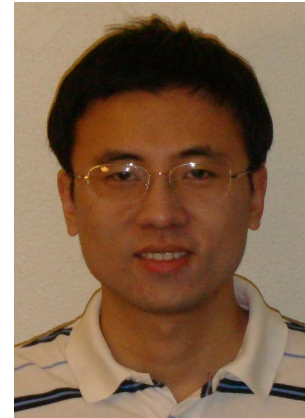
- STRUCTURED OPTIMAL CONTROL OF VEHICULAR FORMATIONS
 - ★ Optimal gains are spatially non-uniform
- PLATOONS:
 - ★ Limitations due to chaining of open-loop integrators
Jovanović & Bamieh, IEEE TAC '05
 - ★ Must have global interactions to address tightness problem
 - ★ Even then, convergence of **Merge & Split Maneuvers** scales badly with N
Jovanović, Fowler, Bamieh, D'Andrea, SCL '08
- FUNDAMENTAL LIMITATIONS FOR SPATIALLY INVARIANT LATTICES
 - ★ Bassam's talk
Bamieh, Jovanović, Mitra, Patterson, IEEE TAC '10 (accepted)

Acknowledgments

TEAM:



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(U of M)

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