

Due Monday 05/13/13 (noon, Xiaofan's office)

1. Khalil, Problem 13.27. (In part (b), do simulations but skip the performance comparison question.)
2. In class, we used the PR Lemma to show that a positive real linear system,

$$\dot{x} = Ax + Bu$$

$$y = Cx$$

has relative degree one, that is,  $CB \neq 0$ . Show that positive realness also implies a minimum phase property. (Hint: Write the system equations in *normal form* and apply Positive Real Lemma.)

3. The dynamics of the *translational oscillator with rotating actuator* (TORA) are described by:

$$\dot{x}_1 = x_2$$

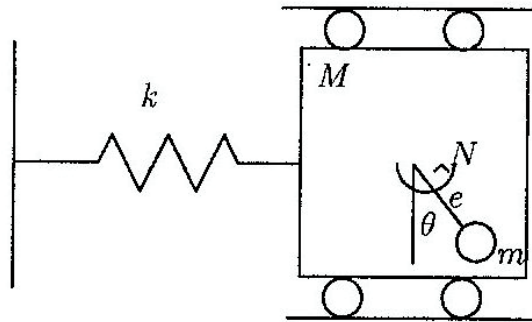
$$\dot{x}_2 = \frac{-x_1 + \epsilon x_4^2 \sin x_3}{1 - \epsilon^2 \cos^2 x_3} + \frac{-\epsilon \cos x_3}{1 - \epsilon^2 \cos^2 x_3} u$$

$$\dot{x}_3 = x_4$$

$$\dot{x}_4 = \frac{1}{1 - \epsilon^2 \cos^2 x_3} (\epsilon \cos x_3 (x_1 - \epsilon x_4^2 \sin x_3) + u)$$

where  $x_1$  and  $x_2$  are the displacement and the velocity of the platform,  $x_3$  and  $x_4$  are the angle and angular velocity of the rotor carrying the mass  $m$ , and  $u$  is the control torque applied to the rotor. The parameter  $\epsilon < 1$  depends on the eccentricity  $e$  and the masses  $m$  and  $M$ .

With  $y = x_3$  as the output, determine the relative degree and the zero dynamics. Provide a physical interpretation of the zero dynamics.



**13.24** Consider the system (13.44)–(13.45), where  $A - BK$  is Hurwitz, the origin of  $\dot{\eta} = f_0(\eta, 0)$  is asymptotically stable with a Lyapunov function  $V_0(\eta)$  such that  $[\partial V_0 / \partial \eta] f_0(\eta, 0) \leq -W(\eta)$  for some positive definite function  $W(\eta)$ . Suppose  $\|\delta\| \leq k[\|\xi\| + W(\eta)]$ . Using a composite Lyapunov function of the form  $V = V_0(\eta) + \lambda \sqrt{\xi^T P \xi}$ , where  $P$  is the solution of  $P(A - BK) + (A - BK)^T P = -I$ , show that, for sufficiently small  $k$ , the origin  $z = 0$  is asymptotically stable.

**13.25** Consider the system

$$\dot{x}_1 = x_2 + 2x_1^2, \quad \dot{x}_2 = x_3 + u, \quad \dot{x}_3 = x_1 - x_3, \quad y = x_1$$

Design a state feedback control law such that the output  $y$  asymptotically tracks the reference signal  $r(t) = \sin t$ .

**13.26** Repeat the previous exercise for the system

$$\dot{x}_1 = x_2 + x_1 \sin x_1, \quad \dot{x}_2 = x_1 x_2 + u, \quad y = x_1$$

**13.27** The magnetic suspension system of Exercise 1.18 is modeled by

$$\begin{aligned} \dot{x}_1 &= x_2 \\ \dot{x}_2 &= g - \frac{k}{m} x_2 - \frac{L_0 a x_3^2}{2m(a + x_1)^2} \\ \dot{x}_3 &= \frac{1}{L(x_1)} \left[ -R x_3 + \frac{L_0 a x_2 x_3}{(a + x_1)^2} + u \right] \end{aligned}$$

where  $x_1 = y$ ,  $x_2 = \dot{y}$ ,  $x_3 = i$ , and  $u = v$ . Use the following numerical data:  $m = 0.1$  kg,  $k = 0.001$  N/m/sec,  $g = 9.81$  m/sec<sup>2</sup>,  $a = 0.05$  m,  $L_0 = 0.01$  H,  $L_1 = 0.02$  H, and  $R = 1$   $\Omega$ .

- Show that the system is feedback linearizable.
- Using feedback linearization, design a state feedback control law to stabilize the ball at  $y = 0.05$  m. Repeat parts (d) and (e) of Exercise 12.8 and compare the performance of this controller with the one designed in part (c) of that exercise.
- Show that, with the ball position  $y$  as the output, the system is input-output linearizable.
- Using feedback linearization, design a state feedback control law so that the output  $y$  asymptotically tracks  $r(t) = 0.05 + 0.01 \sin t$ . Simulate the closed-loop system.

, and  $F_y$ , show

$$\begin{bmatrix} L^2 & mL \cos \theta \\ s \theta & M + m \end{bmatrix}$$

$$\begin{bmatrix} u \\ \sin \theta - kx_c \end{bmatrix}$$

$$[ + mI > 0$$

les and  $u$  as the

RA) system.

ing its voltage,  $v_a$  are the corre- l equation. The

third equation is a torque equation for the shaft, with  $J$  as the rotor inertia and  $c_3$  as a damping coefficient. The term  $c_1 i_f \omega$  is the back e.m.f. induced in the armature circuit, and  $c_2 i_f i_a$  is the torque produced by the interaction of the armature current with the field circuit flux.

- (a) For a separately excited DC motor, the voltages  $v_a$  and  $v_f$  are independent control inputs. Choose appropriate state variables and find the state equation.
- (b) Specialize the state equation of part(a) to the field controlled DC motor, where  $v_f$  is the control input, while  $v_a$  is held constant.
- (c) Specialize the state equation of part(a) to the armature controlled DC motor, where  $v_a$  is the control input, while  $v_f$  is held constant. Can you reduce the order of the model in this case?
- (d) In a shunt wound DC motor, the field and armature windings are connected in parallel and an external resistance  $R_x$  is connected in series with the field winding to limit the field flux; that is,  $v = v_a = v_f + R_x i_f$ . With  $v$  as the control input, write down the state equation.

**1.18** Figure 1.26 shows a schematic diagram of a magnetic suspension system, where a ball of magnetic material is suspended by means of an electromagnet whose current is controlled by feedback from the, optically measured, ball position [211, pp. 192-200]. This system has the basic ingredients of systems constructed to levitate mass, used in gyroscopes, accelerometers, and fast trains. The equation of motion of the ball is

$$m\ddot{y} = -k\dot{y} + mg + F(y, i)$$

where  $m$  is the mass of the ball,  $y \geq 0$  is the vertical (downward) position of the ball measured from a reference point ( $y = 0$  when the ball is next to the coil),  $k$  is a viscous friction coefficient,  $g$  is the acceleration due to gravity,  $F(y, i)$  is the force generated by the electromagnet, and  $i$  is its electric current. The inductance of the electromagnet depends on the position of the ball and can be modeled as

$$L(y) = L_1 + \frac{L_0}{1 + y/a}$$

where  $L_1$ ,  $L_0$ , and  $a$  are positive constants. This model represents the case that the inductance has its highest value when the ball is next to the coil and decreases to a constant value as the ball is removed to  $y = \infty$ . With  $E(y, i) = \frac{1}{2}L(y)i^2$  as the energy stored in the electromagnet, the force  $F(y, i)$  is given by

$$F(y, i) = \frac{\partial E}{\partial y} = - \frac{L_0 i^2}{2a(1 + y/a)^2}$$

When the electric circuit of the coil is driven by a voltage source with voltage  $v$ , Kirchhoff's voltage law gives the relationship  $v = \dot{\phi} + Ri$ , where  $R$  is the series resistance of the circuit and  $\phi = L(y)i$  is the magnetic flux linkage.

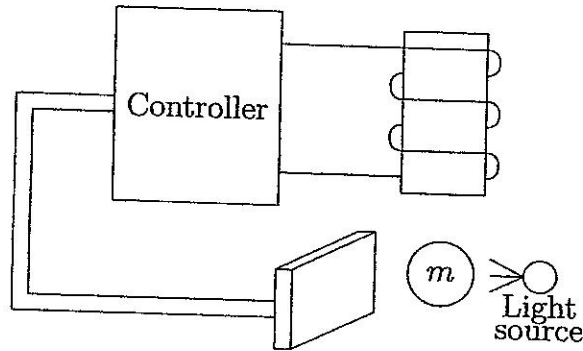


Figure 1.26: Magnetic suspension system of Exercise 1.18.

- (a) Using  $x_1 = y$ ,  $x_2 = \dot{y}$ , and  $x_3 = i$  as state variables and  $u = v$  as control input, find the state equation.
- (b) Suppose it is desired to balance the ball at a certain position  $\tau > 0$ . Find the steady-state values  $I_{ss}$  and  $V_{ss}$  of  $i$  and  $v$ , respectively, which are necessary to maintain such balance.

The next three exercises give examples of hydraulic systems [41].

**1.19** Figure 1.27 shows a hydraulic system where liquid is stored in an open tank. The cross-sectional area of the tank,  $A(h)$ , is a function of  $h$ , the height of the liquid level above the bottom of the tank. The liquid volume  $v$  is given by  $v = \int_0^h A(\lambda) d\lambda$ . For a liquid of density  $\rho$ , the absolute pressure  $p$  is given by  $p = \rho gh + p_a$ , where  $p_a$  is the atmospheric pressure (assumed constant) and  $g$  is the acceleration due to gravity. The tank receives liquid at a flow rate  $w_i$  and loses liquid through a valve that obeys the flow-pressure relationship  $w_o = k\sqrt{\Delta p}$ . In the current case,  $\Delta p = p - p_a$ . Take  $u = w_i$  to be the control input and  $y = h$  to be the output.

- (a) Using  $h$  as the state variable, determine the state model.
- (b) Using  $p - p_a$  as the state variable, determine the state model.
- (c) Find  $u_{ss}$  that is needed to maintain the output at a constant value  $\tau$ .

**1.20** The hydraulic system shown in Figure 1.28 consists of a constant speed centrifugal pump feeding a tank from which liquid flows through a pipe and a valve that obeys the relationship  $w_o = k\sqrt{p - p_a}$ . The pump characteristic for the specified pump speed is shown in Figure 1.29. Let us denote this relationship by  $\Delta p = \phi(w_i)$  and denote its inverse, whenever defined, by  $w_i = \phi^{-1}(\Delta p)$ . For the current pump,  $\Delta p = p - p_a$ . The cross-sectional area of the tank is uniform; therefore,  $v = Ah$  and  $p = p_a + \rho gv/A$ , where the variables are defined in the previous exercise.